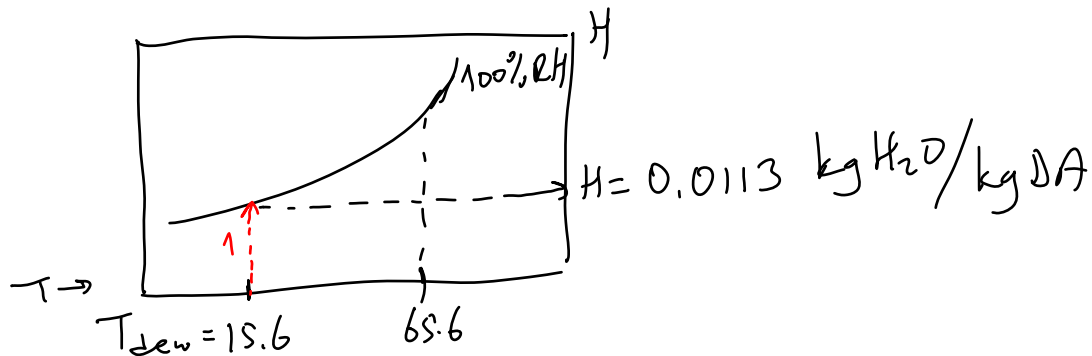


PROBLEMS

1) The air entering a dryer has a temperature of 65.6°C and dew point of 15.6°C . Calculate the humid volume and humid heat of this mixture.

Solution:

$$T = 65.6 + 273 = 338.6 \text{ K}$$



⊗ Humid Volume, $v_H = (2.83 \times 10^{-3} + 4.56 \times 10^{-3} \times H) \times T^{\rightarrow \text{K}}$

$$v_H = (2.83 \times 10^{-3} + 4.56 \times 10^{-3} \times 0.0113) \times (338.8)$$

$$= 0.976 \text{ m}^3 \text{ wet air / kg DA}$$

⊗ Humid Heat, $C_s = (1.005 + 1.88 \times H)$

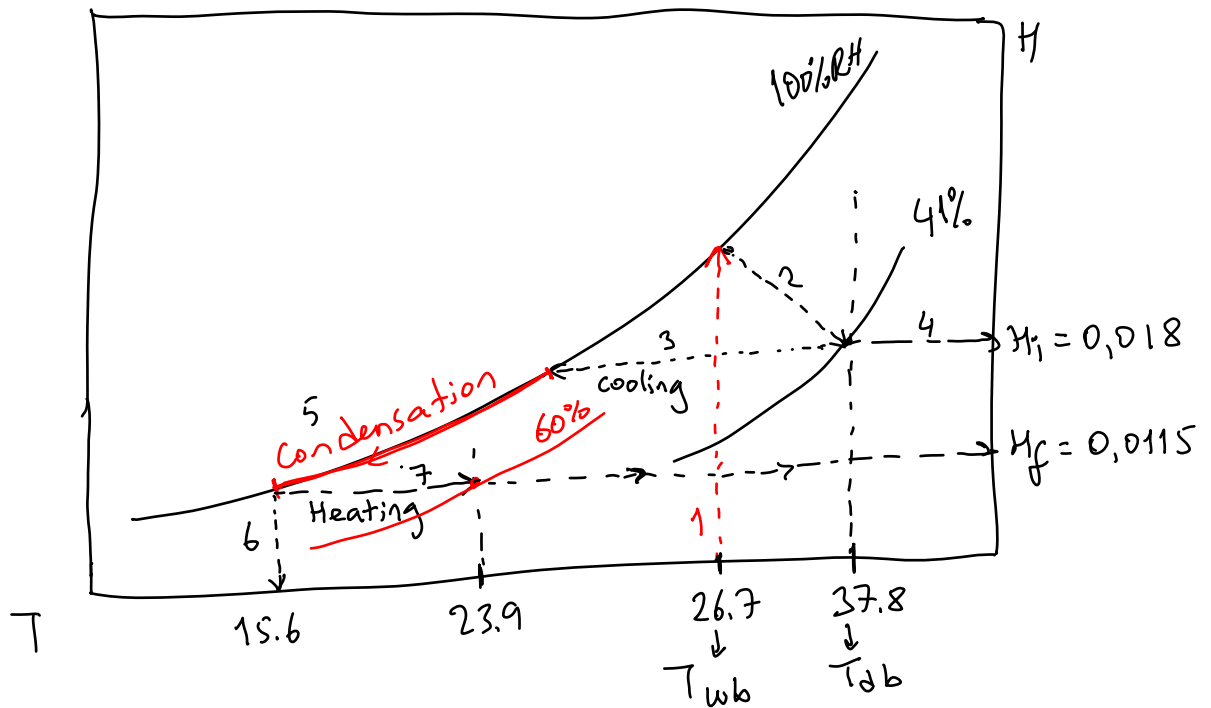
$$= 1.005 + 1.88 \times 0.0113 = 1.026 \text{ kJ/kg DA}$$

2) Air having a dry bulb temperature of 37.8°C and a wet bulb of 26.7°C is to be dried by first cooling to 15.6°C to condense water vapor and then heating to 23.9°C .

a) Calculate the initial absolute humidity and relative humidity

b) Calculate the final absolute humidity and relative humidity

Solution:



a) $H_i = 0,018 \text{ kgH}_2\text{O}/\text{kgDA}$, $RH = 41\%$.

b) $H_f = 0,0115 \text{ kgH}_2\text{O}/\text{kgDA}$, $RH = 60\%$

3) A tunnel dryer is being designed for drying apple halves from an initial moisture content of 70 % (wb) to a final moisture content of 5 % (wb). An experimental drying curve for the product indicates that the critical moisture content is 25 % (wb) and the time for constant rate drying is 5 min. Based on the information provided, estimate the total drying time for the product. Assume 1 kg of dry solids/m² of effective drying surface as the basis. Assume a straight line of the rate R vs X passes through the origin.

Solution:

$$X_1 = \frac{70}{30} = 2.33 \text{ kgH}_2\text{O}/\text{kgDS}$$

$$X_c = \frac{25}{75} = 0.333 \quad "$$

$$X_2 = \frac{5}{95} = 0,0526 \quad "$$

$$t_c = 5 \text{ min (given)}, \quad \frac{Ls}{A} = 1 \frac{\text{kgDS}}{\text{m}^2} \text{ (given)}$$

$$R_c = \frac{L_s \times (X_1 - X_2)}{A \times t_c} = 1 \times \frac{(2.33 - 0.333)}{5} \Rightarrow$$

$$R_c = 0.4 \text{ kg H}_2\text{O}/(\text{m}^2 \cdot \text{min})$$

$$t_f = \frac{L_s}{A} \times \frac{X_c}{R_c} \times \ln \frac{X_c}{X_2} = 1 \times \frac{0.333}{0.4} \times \ln \left(\frac{0.333}{0.0526} \right) \Rightarrow$$

$$t_f = 1.54 \text{ min}$$

$$\text{Total drying time} = t_c + t_f = 5 + 1.54 = 6.54 \text{ min.}$$

4) A bed of material consisting of wet granular solids is being dried in a current of heated air. The air is maintained at a temperature of 338 K (65°C) and a relative humidity of 15 %. Assuming that no shrinkage takes place, then, calculate the depth of a bed of this material which will take 12 hours to dry from an initial moisture content of 1.0 kg H₂O/kg dry solids to a final moisture content of 0.1 kg H₂O/kg dry solids.

Additional data:

Critical MC: 0.5 kg H₂O/kg dry solids

Equilibrium MC: 0.02 kg H₂O/kg dry solids

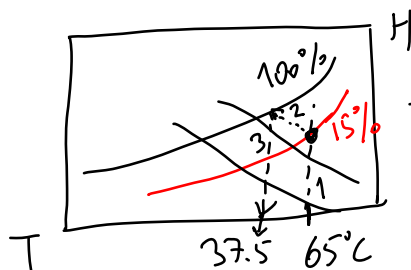
Bulk density of the dry solids: 1600 kg/m³

The heat transfer coefficient to the surface during the constant rate period was found to be 162 kJ/(h.m².K).

Solution:

For through circulation drying where the drying gas passes upward or downward through a bed of wet granular solids, both a constant rate period and a falling rate period of drying may result. Often the granular solids are arranged on a screen so that the gas passes through the screen and through the open spaces or voids between the solid particles.

Solution:



$$\Rightarrow T_s = T_{wb} = 37.5^\circ\text{C}, \lambda_w = ? \text{ at } 37.5^\circ\text{C}$$

From saturated steam table;

$$\lambda_w = 2410.3 \text{ kJ/kg H}_2\text{O}$$

For such drying processes \Rightarrow

$$t_c = \frac{\rho_s \times \lambda_w \times d \times (X_1 - X_c)}{(T - T_{wb}) \times h} \quad , \quad d: \text{depth of bed.}$$

$$t_f = \frac{\rho_s \times \lambda_w \times d \times (X_c - X_e)}{(T - T_{wb}) \times h} \times \ln \left[\frac{X_c - X_e}{X_2 - X_e} \right]$$



$$t_{\text{total}} = t_c + t_f = 12 \text{ hr (Given)} \Rightarrow$$

$$12 = \frac{1600 \times 2410,3 \times d \times (1 - 0,5)}{(338 - 310,5) \times 162} + \frac{1600 \times 2410,3 \times d \times (0,5 - 0,02)}{(338 - 310,5) \times 162} \times \ln \left[\frac{0,5 - 0,02}{0,1 - 0,02} \right]$$

\searrow
 $37,5^\circ\text{C}$

$$\Rightarrow d = 0,0102 \text{ m} \equiv 1,02 \text{ cm}$$

5) 100 kg of food material are dried from an initial water content of 80 % on a wet basis and with an effective surface drying area of 12 m². Estimate the time needed to dry to 50 % moisture content on a wet basis, assuming constant rate drying period in air at a temperature of 120°C dry bulb and 50°C wet bulb. Under the conditions in the drier, measurements indicate the convective heat transfer coefficient to the food surface from the air to be 18 J/(m².s.°C).

Solution:

$$t_c = \frac{L_s \times \lambda_w \times (X_1 - X_2)}{A \times h \times (T - T_{wb})} \quad , \quad T_{wb} \cong T_{\text{sat.}}$$

$$X_1 = \frac{80}{100-80} = 4 \text{ kg H}_2\text{O/kg DS}$$

$$X_2 = \frac{50}{100-50} = 1 \text{ kg H}_2\text{O/kg DS}$$

$$T_{wb} = 50^\circ\text{C} \Rightarrow \lambda_w \text{ at } 50^\circ\text{C} = 2383 \frac{\text{kJ}}{\text{kg H}_2\text{O}} \text{ from sat'd steam table.}$$

$$h = 18 \frac{\text{J}}{\text{m}^2 \cdot \text{s} \cdot ^\circ\text{C}} \times \frac{1 \text{kJ}}{1000 \text{J}} = 18 \times 10^{-3} \text{ kJ}/(\text{m}^2 \cdot \text{s} \cdot ^\circ\text{C})$$

$$L_s = 100 \times (1 - 0.8) = 20 \text{ kg DS.}$$

$$t_c = \frac{20 \text{ kg DS} \times 2383 \frac{\text{kJ}}{\text{kg H}_2\text{O}} \times (4 - 1) \frac{\text{kg H}_2\text{O}}{\text{kg DS}}}{12 \text{ m}^2 \times 18 \times 10^{-3} \frac{\text{kJ}}{\text{m}^2 \cdot \text{s} \cdot ^\circ\text{C}} \times (120 - 50) ^\circ\text{C}}$$

$$t_c = 9456 \text{ s} \times \frac{1 \text{ hr}}{3600 \text{ s}} \approx 2.63 \text{ h}$$

6) 2060 lb/h of dried product (with 4 % wet basis moisture) is produced from a co-current drier. Atmospheric air (75°F) of absolute humidity $H_1=0.0095$ kg water/kg dry air is heated to 350°F before entering the drier. Air is exhausted from the drying chamber at 176°F. Feed contains 45 % solids and pumped in to the dryer at 80°F. Dried product temperature is 115°F. What is the dry air flow rate and absolute humidity of air outlet if no heat loss from the drying system.

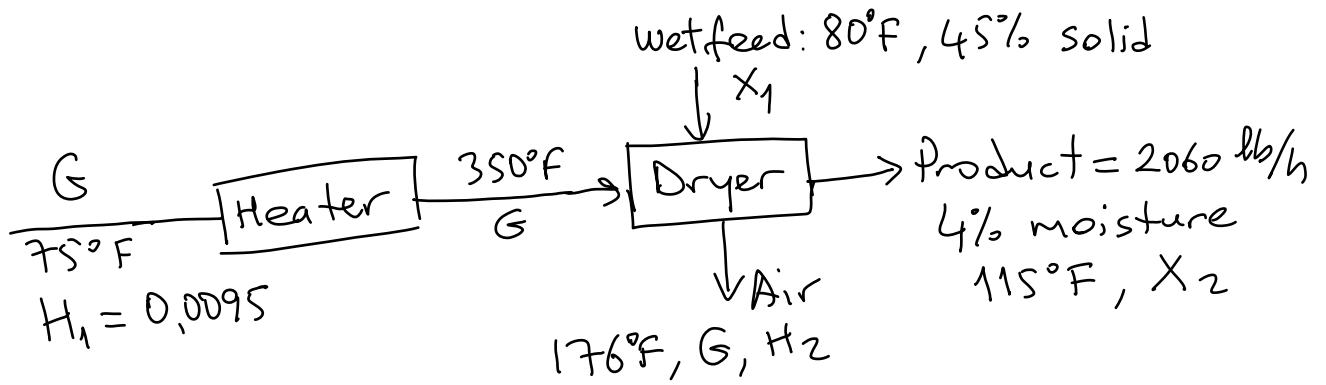
$$C_s = 0.24 + 0.45xH, \text{ Btu}/(\text{lb DA} \cdot ^\circ\text{F})$$

Latent heat of water at 32°F: 1075 Btu/lb water

Specific heat of dry product: 0.40 Btu/(lb dry solids.°F)

Specific heat of water: 1 Btu/lb water.°F

Solution:



$$L_s = 2060 \frac{\text{lb}}{\text{h}} \times 0.96 = 1977.6 \text{ lb DS/h}$$

$$X_1 (\text{d.b.}) = \frac{0.55}{1 - 0.55} = 1.22 \text{ lb H}_2\text{O/lb DS}$$

$$X_2 (\text{d.b.}) = \frac{0.04}{1 - 0.04} = 0.0416 \text{ lb H}_2\text{O/lb DS}$$

Material balance for H₂O on dryer:

$$G \cdot H_1 + L_s \cdot X_1 = G \cdot H_2 + L_s \cdot X_2$$

$$G \cdot 0.0095 + 1977.6 \cdot 1.22 = G \cdot H_2 + 1977.6 \cdot 0.0416 \Rightarrow$$

$$\boxed{0.0095G + 2330.4 = GH_2} \rightarrow \text{eqn (1)}$$

Heat balance on dryer:

$$H'_{G_1} = C_s (T_G - T_0) + H \cdot \overset{\text{at } 32^\circ\text{F}}{L_0} \rightarrow \text{for gas}$$

$$H'_s = C_{p_s} (T_s - T_0) + X \cdot C_{p_w} (T_s - T_0) \rightarrow \text{for solid.}$$

$$G \cdot H'_{G_1} + L_s \cdot H'_s = G \cdot H'_{G_2} + L_s \cdot H'_{s_2} + \cancel{Q_{\text{Loss}}} \rightarrow 0$$

$$G \times [(0.24 + 0.45 \times 0.0095)(350 - 32) + 0.0095 \times 1075.2] + 1977.6 [0.40(80 - 32) + 1.22 \times 1 \times (80 - 32)] = G \times [(0.24 + 0.45 \times H_2)(176 - 32) + H_2 \times 1075.2] + 1977.6 [0.40 \times (115 - 32) + 0.0416 \times 1 \times (115 - 32)] \Rightarrow$$

$$87.8G + 153778.18 = G(34.56 + 64.8H_2 + 1075.2H_2) + 72484.5 \Rightarrow$$

$$87.8G + 81293.59 = 1140G \cdot H_2 + 34.56G$$

$$53.24G + 81293.59 = 1140GH_2 \rightarrow \text{eqn (2)}$$

Substituting eqn (1) into eqn (2)

$$53.24G + 81293.59 = 1140[0.0095G + 2330.4] \Rightarrow$$

$$42.41G = 2575362.2 \Rightarrow$$

$$G = 60725.35 \text{ lb dry air/h}$$

$$GH_2 = 0.0095 \times G + 2330.4 \rightarrow \text{eqn (1)}$$

$$H_2 = 0.0478 \text{ lb H}_2\text{O/lb DA}$$

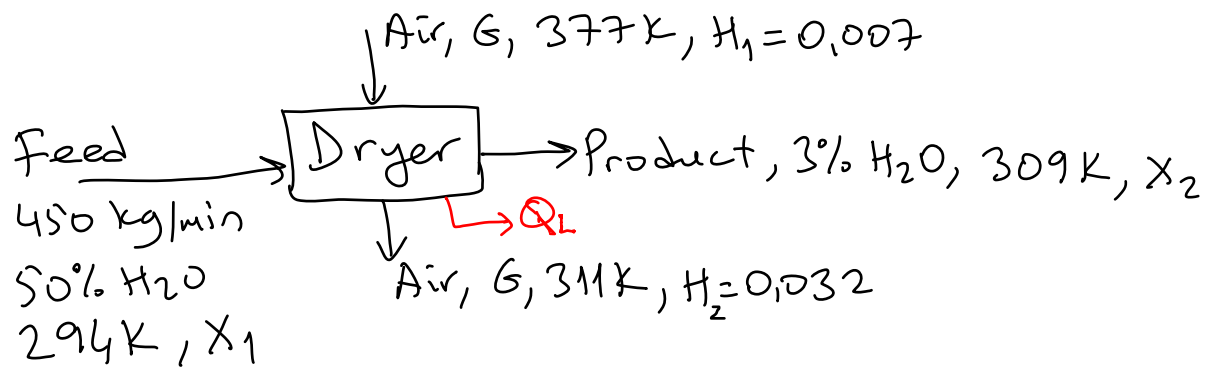
7) 450 kg/min of a feed material containing 50 % moisture (wet weight basis) enters a drier at 294K. The product containing 3 % moisture (wet weight basis) leaves the drier at 309K. The air enters the drier at 377K with an absolute humidity of 0.007 kg water/kg dry air. The air leaves the drier at 311K. Calculate heat loss, % heat loss and weight of dry air used per hour. The humidity of air leaving the drier is 0.032 kg water/kg dry air.

Cp (liquid water): 4.19 kJ/kg.K, Cp (solid): 0.83 kJ/kg.K

Cp (water vapor): 2 kJ/kg.K, Cp (air): 0.95 kJ/kg.K

Latent heat of vaporization of water at 273K: 2411 kJ/kg

Solution:



$$Q_{\text{Loss}} = ? , G = ? \text{ (kg/h)}$$

$$\text{Dry solids, } L_s = 450 \times 0.5 = 225 \frac{\text{kg DS}}{\text{min}} \times \frac{60 \text{ min}}{1 \text{ hr}} = 13500 \frac{\text{kg DS}}{\text{h}}$$

$$X_1 = \frac{0.50}{1 - 0.5} = 1 \text{ kg } H_2O / \text{kg DS}$$

$$X_2 = \frac{0.03}{1 - 0.03} = 0.0309 \text{ kg } H_2O / \text{kg DS}$$

Material balance for H_2O on dryer:

$$G \times H_1 + L_s \times X_1 = G \times H_2 + L_s \times X_2$$

$$G \times 0.007 + 225 \times 1 = G \times 0.032 + 225 \times 0.0309$$

$$0.025G = 218.05 \Rightarrow$$

$$G = 8722 \frac{\text{kg DA}}{\text{min}} \times \frac{60 \text{ min}}{\text{h}} = 523320 \frac{\text{kg DA}}{\text{h}}$$

Heat balance on dryer:

$$G \times H'_{G_1} + L_s \times H'_{S_1} = G \times H'_{G_2} + L_s \times H'_{S_2} + Q_{\text{Loss}}$$

$$523320 \times [(0.95 + 2 \times 0.007) \times (377 - 273) + 0.007 \times 2411] +$$

$$13500 \times [0.83(294 - 273) + 1 \times 4.19 \times (294 - 273)] =$$

$$523320 \times [(0,95 + 2 \times 0,032) \times (311 - 273) + 0,032 \times 2411] + 13500 \times [0,83(309 - 273) + 0,0309 \times 4,19(309 - 273)] + Q_{Loss}$$

$$\Rightarrow 62718071 \frac{\text{kJ}}{\text{h}} = 61006053 \frac{\text{kJ}}{\text{h}} + Q_{Loss}$$

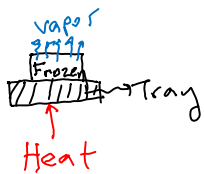
$$Q_{Loss} = 1712018 \text{ kJ/h}$$

$$\% Q_{Loss} = \frac{1712018}{62718071} \times 100 \approx 2,73\%$$

8) A slab of frozen orange juice to be freeze dried, from a moisture content of 87 % to 3% (db). The slab, 1.2 cm thick, rests on a tray and is heated by radiation from upper surface. The source of radiation is regulated so as to maintain the surface temperature at 30°C at all times. The frozen juice is at - 18°C. The latent heat of sublimation is 3000 kJ/kg. The thermal conductivity of the dry layer at the pressure of operation is 0.09 W/(m.K). The density of the frozen juice is 1000 kg/m³. Estimate the drying time.

Solution:

$$t = \frac{L_s \times \rho \times (X_0 - X_f)}{k \times (T_s - T_f)} \times \frac{L^2}{2}, \quad \begin{matrix} L = 1,2 \text{ cm} \\ = 0,012 \text{ m} \end{matrix}$$



$$= \frac{3000 \times 10^3 \text{ J/kg H}_2\text{O} \times 1000 \frac{\text{kg solid}}{\text{m}^3} \times (0,87 - 0,03) \frac{\text{kg H}_2\text{O}}{\text{kg OS}} \times \frac{(0,012 \text{ m})^2}{2}}{[30 - (-18)] \text{ K} \times 0,09 \frac{\text{J}}{\text{s} \cdot \text{m} \cdot \text{K}}}$$

$$\Rightarrow t = 42000 \text{ s} \approx 11,67 \text{ h}$$

9) Slices of a food product 5 mm thick are freeze-dried from both major surfaces of the slices, kept at 50°C, in the vacuum chamber. The chamber pressure is 60 Pa and pressure at ice front is 85 Pa. The temperature of ice

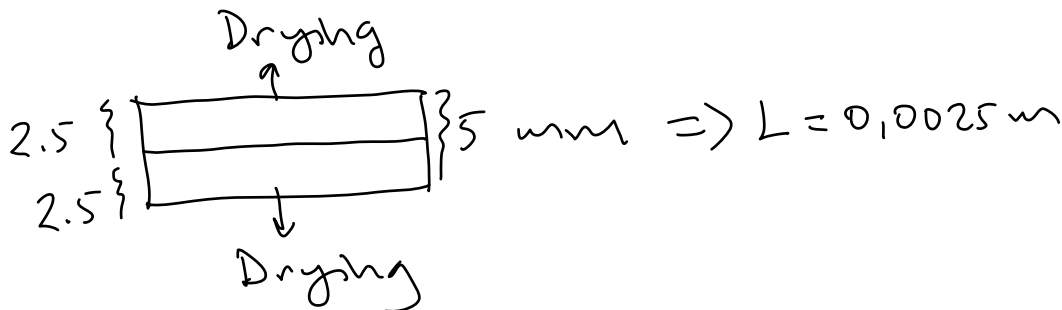
is - 22 °C. Calculate the time to dry from 200 % (db) moisture content to 5 % (db).

k: 0.02 W/(m.K), b: 2×10^{-8} kg/(s.m.Pa)

Ls: 2.95×10^6 J/kg, density: 500 kg/m³.

Solution:

$$t = \frac{L_s \times \rho \times (X_0 - X_f)}{k \times (T_s - T_f)} \times \frac{L^2}{2}$$



$$t = \frac{2.95 \times 10^6 \times 500 \times (2 - 0.05)}{0.02 \times [50 - (-22)]} \times \frac{(0.0025)^2}{2} \Rightarrow$$

$$t = 5837 \text{ sec} \approx 1.62 \text{ h}$$

OR

$$t = \frac{\rho \times (X_0 - X_f) \times \frac{L^2}{2}}{b \times \underbrace{(P_i - P_0)}_{\Delta P}}$$

P_i : Vapor P at ice front
 P_0 : " " " dried layer
 Surface (top) and Surface (bottom)

$$t = \frac{500 \times (2 - 0.05) \times (0.0025)^2 / 2}{2 \times 10^{-8} \times (85 - 60)} = 3808 \text{ sec} \approx 1.06 \text{ h}$$